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IN THE U.S. PATENT AND TRADEMARK OFFICE

Appl. No. : 10/519,577
Applicant : Levner, et al.
Filed : Dec 27, 2004
TC/AU : 2874
Examiner : Pak, Sung H.

Docket No. : 904.0102.U1(US)
Customer No. : 29683

Title : METHOD AND APPARATUS FOR DETECTING MULTIPLE OPTICAL
WAVE LENGTHS

Mail Stop Petition
Commissioner for Patents
P.O. Box 1450
Alexandria, VA 22313-1450

PETITION FOR BENEFIT UNDER 35 USC §120

Sir:

Applicant hereby petitions the Commissioner to allow the Applicants of the above identified application to claim benefit as a continuation in part of co-pending non-provisional application serial number 10/188,530 under 35 USC 120 and 37 CFR 1.53(b). The Applicants present the following items with this Petition to satisfy the showing under 37 CFR 1.78(3) and related paragraphs:

- 1.78(a)(1)(i): This application is a US National Stage entry from PCT/US2003/20237 (int'l filing date June 27, 2003, priority to June 27, 2002) which designated the United States [see paras (22), (30), (81) of the published PCT application WO 2004/003598 A1].
- 1.78(a)(2)(i): This petition seeks to amend the written description to claim priority as required by this provision. Co-pendency is satisfied as of the date of this petition. An amendment is submitted to the Examiner on the same date as

this petition, entry of such pending a decision on this petition. A copy of that amendment is attached hereto.

- 1.78(a)(3)(i): A copy of Application No. 10/188,530 as filed is attached hereto.
- 1.78(a)(3)(ii): A draft in the amount of \$1370 under 1.17(t) is attached. The Patent Office is authorized to charge Deposit Account No. 50-1924 for any discrepancy between the amount due and the amount enclosed.
- 1.78(a)(3)(iii): The undersigned attests, on knowledge and belief after reviewing the attorney files for both the subject application and that to which benefit claim is petitioned, that the entire delay between the date that the benefit claim was due under 1.78(a)(2)(i) and the date of this petition was unintentional.

Specifically, the subject application claims priority, through the PCT application from which national stage was entered, to ser. no. 60/392,306 (filed June 27, 2002) and ser. no. 60/393,209 (filed July 1, 2002). Application ser. no. 10/188,530 claims priority to ser. no. 60/302,904 (filed July 3, 2001). It appears that the PCT application claimed priority to only those documents that fully supported the claims of that PCT, and thereby inadvertently failed to claim priority to those applications (10/188,530 and 60/302,904) for which all claims of the PCT application were not fully supported. That this failure was not corrected upon entry into the US national stage was also inadvertent. Only upon citation of US 2003/0007733 (the published application of 10/188,530) in the Office Action dated 4/6/2006 was it brought to the attention of the Applicants and their representative Harrington & Smith LLP that benefit of the subject application under 35 USC 120 and 37 CFR 1.53(b) (continuation-in-part) was not of record before the US Patent Office.

Such benefit is proper at least for the following facts. Application 10/188,530 lists two inventors Daniel Levner and Martin F. Fay. The subject application lists those same two inventors and another, Jingming Xu. The subject matter concerns similar art and the subject application significantly expands on that disclosed in ser. no. 10/188,530.

Specifically:

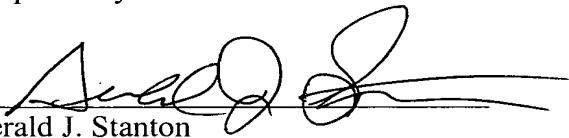
page 9 line 17 through page 20 line 20 of the subject application is substantially identical to paras 0060-0062 of US 2003/0007733 (the publication of 10/188,530);

page 10 line 22 through page 12 line 18 of the subject application is substantially identical to paras 0067-0070 of US 2003/0007733; and

Figures 9, 10, 19, 24a and 25a of the subject application are substantially similar to respective Figures 3, 2, 10, 4A, 9 and 5 of US 2003/0007733.

The above is seen to show that the subject application is properly a continuation-in-part of 10/188,530, and that the entire delay in making this benefit claim was inadvertent. The Commissioner is respectfully entreated to grant this petition so as to allow entry of the amendment to the specification which is attached hereto and submitted separately to the Examiner (submitted along with a copy of this petition).

Respectfully submitted:


Gerald J. Stanton
Reg. No.: 46,008

August 4, 2006
Date

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CERTIFICATE OF MAILING

I hereby certify that this correspondence is being deposited with the United States Postal Service as first class mail in an envelope addressed to: Commissioner for Patents, P.O. Box 1450, Alexandria, VA 22313-1450.

August 4, 2006
Date


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904.0010.U1 (US)

COPY

Patent Application Papers Of:

Daniel Levner

Martin Fay

For: Method and Apparatus for Processing Optical Signals.
With Supergratings



Method and Apparatus for Processing Optical Signals With Supergratings

CLAIM OF PRIORITY FROM COPENING PROVISIONAL PATENT APPLICATIONS

5 Priority is herewith claimed under 35 U.S.C. §119(e) from
co-pending provisional patent application 60/302,904,
filed 7/03/2001, entitled "Method and Apparatus for
Detecting Optical Signals With Binary Supergratings", by
Daniel Levner and Martin Fay. The disclosure of said
10 provisional patent application is incorporated by
reference in its entirety.

Priority is herewith claimed under 35 U.S.C. §119(e) from
co-pending provisional patent application S/N
15 _____ filed 7/01/2002, entitled "Method and
Apparatus for Detecting Multiple Optical Wavelengths", by
Daniel Levner and Martin Fay, Attorney Docket Number
904.0102.P1(US). The disclosure of said provisional
patent application is incorporated by reference in its
20 entirety.

CROSS-REFERENCE TO RELATED APPLICATIONS

This application is also related to co-pending U.S.
25 Application No. _____ (Attorney Docket No.
015A.0002.U2(US) filed May 22, 2002, entitled "Synthesis
of Supergratings", by Daniel Levner, Martin Fay, and
Jingming Xu. The disclosure of this non-provisional
Patent Application is incorporated by reference herein in
30 its entirety.

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates generally to processing optical signals, and more particularly to routing, filtering and detecting optical signals.

2. Prior Art

Gratings are optical devices used to achieve wavelength-dependent characteristics by means of optical interference effects. These wavelength-dependent optical characteristics can, for instance, serve to reflect light of a specific wavelength while transmitting or refracting light at all other wavelengths. Such characteristics are useful in a wide range of situations, including the extraction of individual wavelength-channels in Wavelength Division Multiplexed (WDM) optical communication systems, or providing wavelength-specific feedback for tunable or multi-wavelength semiconductor lasers. Gratings are usually implemented by modulating (varying) the effective index of refraction of a waveguiding structure. These changes in index of refraction cause incident light wavelengths to be reflected or refracted: in the case of an abrupt interface between two index values, light incident directly on the interface is reflected according to the well-known Fresnel reflection law.

The term "multi-wavelength grating" generally refers to a grating that is capable of exhibiting optical characteristics at a number of wavelengths. For example, a multi-wavelength grating may be a grating that reflects light at several select wavelengths (which may correspond

to specific optical communication channels), yet is transparent to light at other wavelengths. In some situations, however, there is a need to set the optical characteristics for a continuous range of wavelengths, rather than at specific wavelength values; for example, when using an optical grating to compensate for the unevenness of optical gain profiles in laser cavities and optical amplifiers. However, achieving this requirement for a continuous range of wavelengths is difficult to meet with traditional grating technologies.

Similarly, a range of optical wavelengths may be used where many communication channels are encoded into a single optical cable by utilizing different wavelengths of light; this is more commonly known as Wavelength Division Multiplexing (WDM) technology. Periodic gratings are often used to separate or process these channels. However, periodic grating technologies process one wavelength, forcing devices intended to process multiple wavelengths to employ multiple single-wavelength periodic gratings. This is not an attractive solution because, on top of the additional losses that each grating creates, even a single grating occupies a considerable amount of space by today's standards of integration and miniaturization. It is thus desired to have a single device capable of processing several wavelengths in a space-efficient manner.

In the field of semiconductor lasers, the output wavelength of semiconductor lasers is largely determined by the presence of "feedback elements" around or inside the laser gain section, which act to reflect light at the desired wavelength back into the laser. For multi-

wavelength operation, multi-wavelength feedback is needed. Again, single-wavelength grating technology can only address this demand with a cascade of simple gratings, leading to the same (if not more notable) loss and space problems mentioned above.

In the field of optical transmission, it is well known that optical networks must contend with a property known as dispersion. This property arises from the wavelength-dependence of effective index, which in turn produces a wavelength-dependent group delay spectrum for a given type and length of optical fiber. Since an optical pulse always possesses some spectral width, this wavelength-dependence leads to different retardation of various spectral components of the optical pulse, thereby leading to its spread in the spatial domain. This spread directly impedes the operation of the optical network. Some forms of dispersion can be corrected for with single-wavelength gratings, but only on a channel by channel basis. More complicated forms of dispersion such as dispersion slope cannot be suitably corrected by single-wavelength gratings at all.

One such single-wavelength grating device is a Bragg Grating. The Bragg Grating consists of a periodic variation in refractive index and acts as a reflector for a single wavelength of light related to the periodicity (known as pitch, Λ) of the index pattern; and is frequently used in both semiconductor systems and fiber-optic systems. In practice, the Bragg Grating can usually reflect at several wavelengths, corresponding to overtones of its fundamental pitch; however, these higher-order wavelengths tend to be at quite different

spectral regions than that of the fundamental wavelength, thus not making the Bragg Grating useful as a multi-wavelength reflector. Moreover, these higher-order wavelengths cannot be tuned independently of one another.

5

Other multi-wavelength grating technologies include: analog superimposed gratings, Sampled Gratings (SG), Super-Structure Gratings (SSG), Chirped Bragg Gratings, Dammann Gratings, Arrayed Waveguide Gratings (AWG),
10 Echelle Gratings and Binary Superimposed Gratings (BSG).

Analog superimposed gratings are a generalization of the Bragg Grating and are rooted in a principle of superposition: a grating profile consisting of the sum of
15 the index profiles of single-wavelength gratings reflects at all of its constituent wavelengths. Such a grating relies on an analog index variation, that is, a refractive index that changes continuously along the grating length. However, it is difficult to inscribe
20 strong analog gratings using the well-known photorefractive effect, since the change of index under illumination varies non-linearly with stronger exposures, making the writing process difficult in semiconductors where surface relief gratings are used. It is also very
25 difficult and generally impractical to reproducibly etch analog features into the surface of the semiconductor. The latter difficulty brought about the introduction of binary gratings, i.e., gratings that rely only on two refractive index values corresponding to the material
30 being etched or not etched, illuminated or not illuminated.

Two representations of multi-wavelength binary gratings are sampled gratings (SG) and superstructure gratings (SSG). The SG is constructed with alternating sections of grating and grating-free regions of the waveguide. The alternating sections produce diffraction spectra consisting of multiple reflectance peaks contained within a (typically) symmetric envelope. The SG is intrinsically limited in the flexibility in the location and relative strength of reflectance peaks, and, because of the large fraction of grating-free space, is also spatially inefficient. The SG is therefore particularly unsuitable where a short grating is required or where waveguide losses are high.

With the super-structure grating (SSG), the grating period is chirped by finely varying the grating pitch, which corresponds to the length of one tooth-groove cycle. This can also be thought of as a sequence of finely tuned phase shifts; common phase profiles include linear and quadratic chirp. Such an implementation in principle allows arbitrary peak positions and relative heights, but only at the expense of extremely high resolution, corresponding to a very small fraction of the size of the grating teeth themselves.

Chirped Bragg Gratings are grating devices targeted at applications such as dispersion compensation and optical pulse compression. Here a Bragg grating's pitch Λ is varied along its length. This produces a wavelength-dependent phase spectrum which can be tailored to provide the desired group delay spectrum: $\tau_g = -d\phi/d\omega$. The delay for a given free-space wavelength λ_0 then follows from the round-

trip distance to where local pitch has λ_0 as its Bragg wavelength: $\tau_g(\lambda_0) = 2n_{eff}z(\lambda_0)$, where $z(\lambda_0)$ is the spatial coordinate at which $\Lambda(z) = \lambda_0/2n_{eff}$. In practice, however, these implementations suffer from excessive group-delay ripple, indicating that the dispersion compensation is not complete.

Dammann Gratings are binary gratings devices wherein the grating features are imposed on some surface and wherein the incident light illuminates the surface at some normal or off-normal angle. The optical wavefront incident on this grating experiences a one-time interaction with the grating features and thereby experiences Raman-Nath type diffraction (as opposed to Bragg diffraction). This device is intended for free-space use and is not easily employed in guided-wave applications. Furthermore, to achieve the wavelength resolution requirements imposed by modern optical communication systems the incident light must be collimated to a very high degree, which can prove difficult in practice.

Arrayed Waveguide Gratings (AWG) are used primarily to spatially separate optical channels in a WDM environment. They operated by dividing input multi-wavelength light between an array of waveguides, wherein each waveguide is of a slightly different optical length. The resulting optical phase differences between the waveguides' respective outputs leads to a wavelength-dependent interference pattern, which with proper design can lead to a separation of wavelength components. In practice, this technology requires vast amounts of semiconductor

real estate and imposes extreme manufacturing constraints.

5 Echelle gratings are also used primarily to spatially
separate optical channels in a WDM environment. Here, a
grating plane is generated by means of defining sub-
wavelength reflective features at various glazing angles
and potentially along some curved plane. The grating
plane is then illuminated with multi-wavelength light,
10 often at an oblique angle, and the individual reflections
add up to substantially separate the wavelength
components. The device tends to be very difficult to
implement in practice, requiring both deep and flat
etching characteristics when implemented in
15 semiconductor.

Prior art regarding binary superimposed grating synthesis
is presented in Ivan A. Avrutsky, Dave S. Ellis, Alex
Tager, Hanan Anis, and J. M. Xu, "Design of widely
20 tunable semiconductor lasers and the concept of Binary
Superimposed Gratings (BSG's)," *IEEE J. Quantum
Electron.*, vol. 34, pp. 729-740, 1998.

Older methods in the prior art address the synthesis of
25 "multi-peak" gratings - i.e., gratings characterized by
reflectance at several "peaks", which can be controlled
in their position and strength. In these methods, a
grating engineer begins with a set of sinusoids, each
sinusoid corresponding to a single reflectance peak and
30 weighted according to that peak's desired relative
strength. These peaks are added together (i.e.
superimposed; hence the BSG is known as a superimposed

grating) to produce an "analog profile". This profile is then digitally quantized by a simple threshold method. For example, if the analog profile value is positive (above a pre-selected reference) then the corresponding
5 BSG segment is a high or binary 1 index value; if it is negative, the corresponding BSG segment is a low or binary zero index value.

However, this approach is inadequate in at least two
10 areas: firstly, the threshold quantization process introduces intermodulation, which largely limits the applicability of BSGs synthesized in this manner to active applications (laser feedback elements and the like). Secondly, this synthesis procedure is limited to
15 multi-peak gratings, and offers little or no control over the individual peak shape. It is also entirely incapable of generating flat-top channels, as desired by some communication applications, and of generating the near-arbitrary reflectance spectra demanded by some gain- and
20 dispersion-compensation schemes.

Other methods for BSG synthesis include trial-and-error methods that are most often computationally difficult and inefficient.

25 Therefore, for detecting optical wavelengths in optical devices it is desirable to provide methods and apparatuses for overcoming the disadvantages noted above.

30 SUMMARY

In accordance with one embodiment of the present invention an optical component including at least one

optical supergrating is provided. The at least one optical supergrating includes a quantized refractive index profile adapted to exhibit a finite plurality of refractive indexes; which in turn are adapted to generate
5 a reflectance spectrum in at least one spectral band.

In accordance with another embodiment of the present invention a method of transmitting at least one optical signal from a first point to a second point is provided.
10 The method includes providing at least one first optical waveguide including an optical component. The optical component includes at least one optical supergrating, having a quantized refractive index profile adapted to exhibit a finite plurality of refractive indexes. The
15 finite plurality of refractive indexes are adapted to generate a reflectance spectrum in at least one spectral band corresponding to a Fourier transformed analog refractive index profile. The method includes transmitting the at least one optical signal through the
20 at least one first optical waveguide; and receiving the at least one optical signal at the second point.

In accordance with another embodiment of the invention an optical component including at least one optical supergrating is provided, wherein the at least one
25 optical supergrating comprises a binary quantized refractive index profile adapted to exhibit a finite plurality of refractive indexes. The indexes are adapted to generate a reflectance spectrum in at least one spectral band.

30 In accordance with another embodiment of the present invention a method of processing at least one optical signal is provided. The method includes providing at

least one optical component having at least one optical supergrating. The at least one optical supergrating includes a quantized refractive index profile adapted to exhibit a finite plurality of refractive indexes adapted to generate optical characteristics in at least one spectral band. The method also includes adapting the at least one optical component to affect the at least one optical signal.

In accordance with another embodiment the invention is also directed towards an optical component including at least one optical supergrating. The at least one optical supergrating includes a binary quantized refractive index profile adapted to exhibit a finite plurality of refractive indexes adapted to generate a reflectance spectrum in at least one spectral band.

The invention is also directed towards a method of monitoring the stability of an optical system. The method includes providing at least one optical component having at least one optical supergrating having a quantized refractive index profile. The quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate optical characteristics in at least one spectral band. The method also includes providing a plurality of optical detectors; providing processing electronics; and adapting the at least one optical component to affect at least one chosen wavelength component to interact with the plurality of optical detectors.

In accordance with another embodiment of the invention, a programmable optical component is provided. The programmable optical component includes at least one

optical supergrating having a quantized refractive index profile adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band.

5 In accordance with another embodiment of the invention an optical component is provided. The optical component includes at least one scattering-reducing optical supergrating having a quantized refractive index profile
10 indexes adapted to generate spectral characteristics in at least one spectral band. The supergrating also has at least one grating feature dimension exceeding grating material wavelength $\lambda_{mat} = \lambda_0/n_{eff}$, and a decay constant of the modal tail less than $1/\lambda_{mat}$ in a predetermined region
15 of the at least one scattering reducing optical supergrating.

In accordance with another embodiment of the invention an optical component is provided. The optical component
20 includes at least one multi-dimensional optical supergrating having a quantized refractive index profile. The quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one
25 spectral band.

The invention is also directed towards an optical coupler system for coupling light between waveguides. The optical coupler includes at least one first optical waveguide and
30 at least one second optical waveguide. The optical coupler also includes at least one optical component optically coupling the light from the at least one first

optical waveguide to the at least one second optical waveguide. The at least one optical component includes a quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band.

In accordance with another embodiment of the invention an optical device is provided. The optical device includes at least one optical waveguide having an optical component for reflecting light within the at least one optical waveguide. The optical component includes a quantized refractive index profile adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band. In addition, the optical component includes an optical circulator having at least one optical port, and optically coupled to the at least one optical waveguide and adapted to direct the reflected light to the at least one optical port.

In accordance with another embodiment of the invention an optical dispersion control system is provided. The system includes at least one first optical waveguide adapted to exhibit wavelength-dependent optical phase characteristics. The at least one optical waveguide includes at least one optical component having a quantized refractive index profile adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band.

In accordance with another embodiment of the invention an optical dispersion control system is provided. The system

includes an optical coupler system for coupling light between waveguides and adapted to exhibit wavelength-dependent optical phase characteristics. The optical coupler system includes at least one first optical waveguide and at least one second optical waveguide. The system also includes at least one optical component optically coupling the light from the at least one first optical waveguide to the at least one second optical waveguide. The at least one optical component includes a quantized refractive index profile adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band.

In accordance with one embodiment of the invention an optical device for separating wavelength components of an optical signal is provided. The optical device includes at least one optical wavelength separation system having at least one first optical waveguide and at least one second optical waveguide. The optical device also includes at least one optical component optically coupling the at least one optical wavelength from the at least one first optical waveguide to the at least one second optical waveguide. The at least one optical component includes a quantized refractive index profile adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band.

The invention is also directed towards a wavelength stability monitor. The wavelength stability monitor includes a wavelength monitor having at least one optical component. The monitor also includes a quantized refractive index profile adapted to exhibit a finite

plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band. The monitor also includes a plurality of optical detectors coupled to the wavelength monitor which are adapted to generate a deviation signal when a monitored wavelength deviates. In addition a controller coupled to the plurality of optical detectors is adapted to generate an electrical signal corresponding to wavelength deviation.

10 The invention is also directed towards an optical wavelength equalizer including at least one optical component. The at least one optical component includes a quantized refractive index profile adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band. The optical component is also adapted to adjust wavelength power per wavelength in an optical signal.

20 In accordance with another embodiment of the invention an optical wavelength monitor is provided. The optical wavelength monitor includes at least one optical component, having a quantized refractive index profile adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band. The at least one optical component is adapted to measure power per wavelength in an optical signal.

30 In accordance with another embodiment of the invention an optical component is provided. The optical component includes at least one programmable optical supergrating.

The invention is also directed towards an optical component comprising at least one tuneable optical supergrating. The tuneable optical supergrating includes a quantized refractive index profile adapted to exhibit a
5 finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band.

The invention is also directed towards an optical component having at least one optical supergrating
10 adapted to effect optical phase characteristics in at least one spectral band.

BRIEF DESCRIPTION OF THE DRAWINGS

15

The foregoing aspects and other features of the present invention are explained in the following description, taken in connection with the accompanying drawings, wherein:

20 Figure 1 is a flow chart showing method steps of one method for synthesizing a BSG incorporated by the invention embodiments presented herein;

25 Figure 2 shows a pictorial view of a counter directional coupler incorporating features of the present invention;

Figure 3 shows a pictorial view of a co-directional coupler incorporating features of the present invention;

Figure 3A shows a pictorial view of a counter-directional symmetrical waveguide coupler incorporating features of the present invention;

5 Figure 4 shows a pictorial view of a dispersion compensator incorporating features of the present invention;

10 Figure 4A shows a pictorial view of a dynamic add/drop filter embodiment incorporating features of the present invention;

15 Figure 4B shows a pictorial view of multiple waveguides coupled with programmable BSGs incorporating features of the present invention;

20 Figure 5 shows a pictorial view of an alternate embodiment of a dispersion compensator incorporating features of the present invention;

Figure 6 shows a pictorial view of a wavelength monitor incorporating features of the present invention;

25 Figure 7 shows a pictorial view of a wavelength monitor incorporating features of the 2D embodiment of the present invention;

30 Figure 8 shows a pictorial view of a wavelength monitor incorporating features of the point scatterer array embodiment of the present invention;

Figure 9 is a diagram of a Lambda router incorporating features of the present invention; and

Figure 10 is a pictorial diagram of an intra-waveguide suppression coupler incorporating features of the invention.

5

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

Although the present invention will be described with reference to the supergrating embodiments as shown in the drawings, it should be understood that the present invention can be embodied in many alternate forms of
10 embodiments, and it is not intended that this invention is limited only to that particular type of embodiment. In alternate embodiments the present invention could be used in any suitable optical device requiring one or more
15 optical gratings.

Starting with supergratings as used here, it will be appreciated that there are three main properties that differentiate the supergrating from other grating technologies. The first is that the supergrating relies
20 on a discrete number of effective refractive index levels. This number is historically 2 and hence the supergrating can take the form of a binary grating, in which case it is known as the Binary Supergrating (BSG). For the sake of clarity and illustration this description
25 will focus on the binary embodiment of the present invention, however, it will be appreciated that in alternate embodiments any suitable number of discrete levels of effective refractive index may be used. The different values of effective refractive index may be
30 attained by varying the real refractive index in any part or in the neighborhood of the supergrating, or by any

other method that varies the effective refractive index experienced by propagating light, and it will be appreciated that many embodiments are possible within the present invention.

5

The second defining property of the supergrating is that the grating resembles a sampled structure characterized by a set of sample points, each associated with a sample region. These sample regions, which may take a variety of shapes, are often referred to as refractive index pixels. The supergratings effective refractive index is substantially fixed within each pixel. This refers to the fact that transitions between the grating's index levels cannot occur at arbitrary positions, but, rather, must occur at boundaries of regions defined by the sample points. Thus, the BSG can be described by a series of (often binary) digits, indicating the refractive index setting at each sample point.

20

The third defining property of the supergrating is that an optical wave-front incident on the grating experiences multiple interactions with the grating features. That is, the supergrating operates in the Bragg diffraction regime.

25

Certain supergrating embodiments utilize a sequential array of refractive index pixels, meaning that each pixel is neighbored by only two other pixels, leading to a natural sense of ordering. Such embodiments are referred to as one-dimensional supergratings, and often utilize pixels in the shape of straight or curved lines, or arrays of boxes or dots arranged along the direction of propagation of incident light. It should be noted that

30

these embodiments include the suitable variation of effective refractive index along the length of any waveguide confining propagation along one dimension.

5 Other supergrating embodiments utilize two-dimensional arrays of refractive index pixels wherein the pixels are situated on the same two-dimensional surface. This surface can be planar or curved. Such embodiments often make use of square or hexagonal pixels that are arranged
10 along a suitable periodic lattice, although it may be appreciated that non-periodic arrangements, non-uniform pixels, or other pixel shapes may be suitable and are within the context of the present invention. It should be noted that these embodiments include the suitable
15 variation of effective refractive index in the span of any waveguide confining propagation along two dimensions.

Additional supergrating embodiments utilize three-dimensional arrays of refractive index pixels. Here, the
20 sample points may be situated anywhere or confined to any particular region of space. Such embodiments often make use of box-like or diamond-like pixels that are arranged along a suitable periodic lattice, although it may be appreciated that non-periodic arrangements, non-uniform
25 pixels, or other pixel shapes may be suitable and are within the context of the present invention.

Referring now to Figure 1, supergrating construction
30 involves several key choices. First, Step 351 Selects the refractive index levels for the optical device, as determined from material parameters and lithographic or photoinscription constraints. Step 352 then determines

the desired sample length, considering the desired wavelength range for the grating and the available lithographic resolution. Step 353 sets total device dimensions for the grating, limited by the available physical space and the technological limitations of the inscribing process. It will be appreciated that the methods described herein are for determining grating patterns for surface-relief gratings; however, in alternate embodiments the methods may be readily adapted to fiber grating patterns. The next step 354 converts the desired grating's reflectance specifications to the Fourier domain using the Fourier approximation. Guided by the Fourier approximation, the designer may initially design the grating by its Fourier spectrum. As will be shown below, this step can also implement feedback to account for various inaccuracies of the approximation in order to improve the final result.

Step 353, the Fourier approximation, is a mathematical relation that relates a grating's reflectance spectrum to one or more periodic reflectance spectra. In other words, single-wavelength gratings have reflectance spectra characterized precisely by their periodic structure, and simple superimposed gratings have reflectance spectra characterized by their wavelength or reflectance spectra components. Therefore, the reflectance spectrum of a grating may be related to the Fourier transform of its structure - the Fourier transform being the standard method for evaluating the "frequency content" or "wavelength content" of a waveform.

The next step 355 is quantization of the analog index profile. Delta-Sigma modulation is one such quantization technique that may be used and can be efficiently implemented. It will be appreciated that in alternate
5 embodiments any suitable quantization technique that conserves Fourier information within a spectral band may be used.

Step 356 determines the supergrating's actual reflectance
10 using an exact technique such as the known transfer matrix method. This calculation determines residual errors of the Fourier approximation, and quantifies an error that can be taken back into the Fourier domain and added to the result of the step 353 if step 357
15 determines that the error exceeds a predetermined threshold. This process can be repeated as necessary, although one repetition is often sufficient. It will be appreciated that any suitable technique for determining error between the desired reflectance characteristics and
20 actual reflectance characteristics may be used.

In accordance with one aspect of the invention, deeper, or more profound, supergrating surface features reduce scattering losses due to radiative cladding modes by
25 occupying a greater distance in the normal direction, which, from Huygens principle and Fourier considerations, leads to more robust phase-matching requirement in the normal dimension; thereby reducing (unwanted) scattering efficiency. More quantitatively, grating features are
30 preferably deep-toothed to a depth exceeding the material wavelength $\lambda_{mat} = \lambda_0 / n_{eff}$, and the decay constant of the modal tail is preferably less than $1/\lambda_{mat}$ in the grating region. In alternate embodiments of the invention, the BSG can be

implemented in the core region at the mode's center. Thus, contributions from the normal extent of the grating are relatively equal, thereby enhancing cancellation of the scattered component.

5

In accordance with another aspect of the invention, grating features and optical characteristics may be varied one or more times after manufacture by employing any means of modifying material or effective refractive index locally or over an area. Several such methods of
10 modifying material or effective refractive index include: affecting the temperature of any part or the neighborhood of the supergrating; electro-optic, magneto-optic, electro-strictive, or magneto-strictive tuning of any
15 part or the neighborhood of the supergrating; optically illuminating, mechanically straining, or injecting current into any part or the neighborhood of the supergrating; incorporating an electrochromic material in any part or the neighborhood of the supergrating;
20 incorporating a liquid crystal or optical polymer material in any part or the neighborhood of the supergrating; promoting chemical reaction or reconfiguration in any part or the neighborhood of the supergrating; or effecting a mechanical translation or
25 reconfiguration of any part or the neighborhood of the supergrating. It will be appreciated that other methods for modifying material or effective refractive index, any one or combination of which are within the context of the present invention.

30

Some embodiments apply one or more methods of modifying material or effective refractive index to the entire supergrating or substantial parts or sections thereof,

thereby effecting a general change in the supergrating's optical features. Such general changes include the strengthening or weakening of features, the enablement or disablement of supergrating features of the supergrating as a whole, the tuning of the optical phase of supergrating features, or the spectral shift of supergrating features. These embodiments address what we term a "tunable supergrating". These tunable supergratings may be used interchangeably with other supergratings to provide additional dynamic functionality in any device or embodiment where the latter are used. This is true in particular for all other device embodiments of the present invention.

Other embodiments apply one or more methods of modifying material or effective refractive index to individual pixels of the supergrating or groups thereof. Such embodiments may achieve spectral changes including the strengthening or weakening of features, the enablement or disablement of supergrating features of the supergrating as a whole, the tuning of the optical phase of the supergrating features, or the spectral shift of supergrating features, generally in greater extent than is possible with tunable supergratings. Furthermore, such embodiments may act to create spectral features that were previously not exhibited by the supergrating, remove spectral features that were previously exhibited, or even change the optical characteristics exhibited by the supergrating within a spectral band entirely. These embodiments address what we term a "programmable supergrating". These programmable supergratings may be used interchangeably with other supergratings to provide additional dynamic or programmable functionality in any

device or embodiment where the latter are used. This is true in particular for all other device embodiments of the present invention. Particularly, embodiments of optical couplers, optical dispersion controllers, optical spatial separators, add/drop filters, lambda routers and wavelength equalizers wherein a programmable supergrating is used are possible, and represent much improved functionality.

Supergrating Coupler

Features of the present invention may be used in evanescent-wave couplers to provide wavelength dependent coupling and direction as well as dispersion compensation. For example, light may be coupled from one waveguide to another waveguide, with a desired spectral response: i.e., light at a given wavelength may be coupled fully, fractionally, or not at all, and with a desired phase.

The coupling embodiments may consist of two or more parallel asymmetric or symmetric waveguides (described below). The asymmetric waveguides have overlapping but differing modes, with differing effective (modal) indices $(n_{eff})_1$ and $(n_{eff})_2$ and different propagation vectors $k_1(\lambda_0) = 2\pi(n_{eff})_1/\lambda_0$ and $k_2(\lambda_0) = 2\pi(n_{eff})_2/\lambda_0$, where λ_0 is free-space wavelength. The effective indices will in general be dependent on wavelength λ_0 . It will be appreciated that the amount of modal overlap and the characteristics of the supergrating will determine the wavelength(s) coupled from one waveguide to another and the direction the wavelength(s) will take once coupled.

Optical coupling may be classified into two general categories: counter-directional and co-directional. Light is said to be coupled co-directionally if the coupled light travels in the same general direction (within 90 degrees of) the input light. Light is said to be counter-directionally coupled if the coupled light travels generally in the opposite direction of the input light. These distinctions are most often very clear in practice as the counter- and co-directions are well defined by the optical waveguides. It should be noted that the same supergrating coupler may be used to couple both co- and counter-directionally, and may do either or both for each wavelength within one or more spectral bands. It is appreciated that while device operation is simpler to describe if only one mode of operation is considered, a device incorporating features of both embodiments simultaneously is within the present invention. It is also appreciated that in accordance with several embodiments of the present invention, the coupling characteristics of supergrating couplers may be varied after manufacture, most often by subjecting the supergrating or supergratings responsible for coupling to some form of optical tuning such as those mentioned previously. Any form of supergrating, including one-dimensional, two-dimensional or three-dimensional, and any particular method of effecting the required effective refractive index values is within the context of the present invention.

Counter-directional Supergrating coupler Embodiments

Referring now to Figure 2 there is shown a pictorial

illustration of a counter-directional supergrating coupler 154 incorporating features of the present invention. For this embodiment, counter-directional coupling will occur for a given input wavelength λ_0 when the index perturbation comprises a spatial frequency of $K_g(\lambda_0) = k_1(\lambda_0) + k_2(\lambda_0)$. Again, this is accomplished by a constructing the supergrating 152, as described above, to emulate the desired spectrum of $K_g(\lambda_0)$ and situating the supergrating 152 between the evanescent-coupled waveguides 151, 153. In this embodiment, the supergrating 152 should preferably be free of spatial frequencies of $2k_1(\lambda_0)$ and $2k_2(\lambda_0)$, as these will produce back-reflection within the respective waveguides (i.e. no coupling), thereby decreasing coupling efficiency and yielding undesired back-reflection. Satisfying this condition requires that waveguide asymmetry be sufficient to avoid any overlaps between grating spatial frequencies (K_g 's) yielding inter-waveguide coupling and those yielding intra-waveguide coupling, over all wavelength range(s) of interest; mathematically, this can be expressed as:

$$k_1(\lambda_1) + k_2(\lambda_1) \neq 2k_1(\lambda_2) \text{ and } k_1(\lambda_1) + k_2(\lambda_1) \neq 2k_2(\lambda_2)$$

where k_1 and k_2 are defined earlier with wavelength-dependent effective indexes, and λ_1 and λ_2 are any combination of wavelengths lying within the range(s) of interest.

In alternate embodiments, optical BSG 152 characteristics may be programmable and/or tuneable by controller 152A and/or tuner 152B, respectively.

Co-directional Supergrating Coupler Embodiment

Referring to Figure 3 there is shown a pictorial

illustration of a co-directional supergrating coupler 164 incorporating features of the present invention. In this embodiment, a desired wavelength λ will couple co-directionally from one waveguide 161 to the other 163, when the respective effective indexes are perturbed with spatial frequency $K_g(\lambda_0) = k_1(\lambda_0) - k_2(\lambda_0)$. This is accomplished by a constructing the supergrating 162, as described above, to emulate the desired spectrum of $K_g(\lambda_0)$ and situating the supergrating between the evanescent-coupled waveguides 161, 163.

In alternate embodiments the supergrating is part of the waveguide or on one or more sides of the waveguide. In addition, alternate embodiments optical BSG 162 characteristics may be changed by programmable controller 162A and/or tuner 162B, respectively.

Symmetric Supergrating Coupler Embodiment

Referring to Figure 3A, it will be appreciated that the symmetric supergrating coupler 164A is a special case of the asymmetric supergrating coupler shown in Figure 2, and performs similar functions as the asymmetric coupler 154 but allows the two waveguides 161A, 163A to be weakly asymmetric or even symmetric in their effective index. Thus, limitations expressed previously may be exceeded, independent of the fact that this would normally lead to intra-waveguide reflection.

In alternate embodiments the supergrating is part of the waveguide or on one or more sides of the waveguide. In addition, alternate embodiments may also change optical BSG 162 characteristics through programmable controller 162A and/or tuner 162B, respectively.

Referring to Figure 10 there is shown a pictorial diagram of an intra-waveguide suppression coupler incorporating features of the invention. For example, a device 106 consisting of two waveguides 101, 102 (symmetric or otherwise) with a BSG 104 situated in between may be static, tunable, or programmable as necessary. Two more BSGs, 103, 105 identical to the first BSG 104, but with opposite contrast (1's become 0's and vice-versa), are placed on either side of the two waveguides 101, 102 such that they mirror the center BSG 104 about the corresponding waveguide.

The principle of operation is as follows: let m_1 be the modal profile of guide 1 and m_2 be the modal profile of guide 2. The coupling coefficients relating the two waveguides can be written to first order in grating strength as:

$$C_{12} \propto \int m_1^* m_2 G_{12} + \int m_1^* m_2 (G_{11} + G_{22}) \cong \int m_1^* m_2 G_{12} ,$$

where G_{12} is the center grating 104 and G_{11} 103 & G_{22} 105 are the gratings on the far side of waveguides 1 and 2, respectively. The second term is negligible because the two side gratings 103, 105 are very far from the corresponding opposite waveguide (more precisely, the opposite waveguide's modal profile is negligible in this region).

However, the coupling coefficient from the first waveguide 101 to itself (corresponding to intra-waveguide reflection) follows:

$$C_{11} \propto \int |m_1|^2 G_{11} + \int |m_1|^2 G_{12} = 0 \quad (\text{because } G_{11} = -G_{22} \text{ and symmetry})$$

The result is identical for the second waveguide 102. The only assumption necessary for the cancellation is that

the modal profiles of both waveguides 101,102 be symmetric (about their waveguide, not necessarily identical to each other) and that the gratings be properly symmetrized about the guide. The cancellation is independent of many material parameters such as the waveguides' effective indices, even if they vary independently.

It will be appreciated that the invention advantageously allows for efficient coupling between neighboring symmetric waveguides, while suppressing intra-waveguide reflection.

It will be further appreciated that the invention advantageously allows for efficient coupling between neighboring symmetric waveguides, while suppressing intra-waveguide reflection. It is appreciated that the invention is equally applicable to asymmetric waveguides, and in alternate embodiments may be the preferred embodiment in light of its relaxation of the design requirements.

Coupler Folding

In another embodiment of the present invention, one supergrating coupler may be folded to make better use of chip real estate. This is done by cascading supergrating couplers. The exact choice of connection order or direction depends on the directionality of coupling of the wavelengths of interest, and a combination of operating modes may be used at one time. The several supergrating couplers may be used together to form one or more improved couplers, or to subject input light to several stages of filtering of processing.

Figure 4 represents a cascaded counter-directional coupler 176 embodiment. In this embodiment wavelength λ_1 is counter-directionally coupled from waveguide 171 to waveguide 173, and again counter directionally coupled from waveguide 173 to waveguide 175. It will be appreciated that waveguide 173 may be adapted to compensate for dispersion in waveguide 171.

In alternate embodiments optical BSG 172 characteristics may be programmed and/or tuned through programmable controller 172A and/or tuner 172B, respectively. Likewise, optical BSG 174 characteristics may be programmed and/or tuned through programmable controller 174A and/or tuner 174B, respectively.

Optical Circulator-based Couplers

Figure 5 illustrates another embodiment of the present invention wherein a supergrating optical coupling between two or more waveguides is achieved by means of a supergrating operating in a reflective mode. Light incident through an input waveguide enters an optical circulator through port 1 and is transmitted through to port 2. At port 2, the light is incident on a supergrating and selectively reflected in amplitude and phase and as a function of wavelength back to port two. The optical circulator acts to direct the light returning to port 2 to port 3, wherein it is collected by an output waveguide. The circulator based embodiment has the advantage that it is very suitable to situations where the waveguides are optical fibers as fiber based circulators are readily available.

optical BSG 184 characteristics may be programmed and/or tuned through programmable controller 184A and/or tuner 184B, respectively.

5 Dispersion Compensator Embodiment

In the field of optical transmission, it is well known that optical networks must contend with a property known as dispersion. This property arises from the wavelength-dependence of effective index, which in turn produces a
10 wavelength-dependent group delay spectrum for a given type and length of optical fiber. Since an optical pulse always possesses some spectral width, this wavelength-dependence leads to different retardation of various spectral components of the optical pulse, thereby leading
15 to its spread in the spatial domain. This spread directly impedes the operation of the optical network.

Chirped Bragg Gratings are grating devices targeted at dispersion compensation. Here a Bragg grating's pitch Λ is
20 varied along its length. This produces a wavelength-dependent phase spectrum which can be tailored to provide the desired group delay spectrum: $\tau_g = -d\phi/d\omega$. The delay for a given free-space wavelength λ_0 then follows from the round-trip distance to where local pitch has λ_0 as its Bragg
25 wavelength: $\tau_g(\lambda_0) = 2n_{eff}z(\lambda_0)$, where $z(\lambda_0)$ is the spatial coordinate at which $\Lambda(z) = \lambda_0/2n_{eff}$. In practice, however, these implementations suffer from excessive group-delay ripple, indicating that the dispersion compensation is not complete.

In the present invention a supergrating emulating the effect of a chirped Bragg grating may be implemented by determining the ideal (analog) input chirp function, as derived from the group delay spectrum $\tau_g(\lambda_0)$ (grating-imposed delay is preferably the opposite of that at the input). The ideal analog profile is then fed into the previously described supergrating quantization filter, producing a quantized profile that emulates the desired phase characteristics. The quantization filter may be further optimized as described above to minimize phase noise.

In other embodiments of the present invention the supergrating may be synthesized directly from the required phase-delay characteristics, for instance by Fourier-based synthesis of the specifications.

Different embodiments of the present invention may comprise supergrating couplers, as described above. These couplers may include co-directional and counter-directional couplers, optical circulator based couplers, folded couplers, or any combination of these, but not limited to these. It is appreciated that any optical transmission or direction method wherein a one or more supergratings affect the transmitted or directed light may support the desired optical phase characteristics and is hence within the context of the present invention.

Alternate embodiments of the present invention may involve one or more supergratings adapted to influence light as it is transmitted through the length of a waveguide. These transmission-based embodiments are particularly useful for optical fiber implementations.

Wavelength Stability Monitor Embodiments

To function properly, optical networks require that channel wavelengths remain within some range of their nominal value. Drifting can be caused by a number of factors, including variations in environmental conditions, device aging, and mechanical disruptions. In certain situations, the incident wavelength channel may remain within the range of nominal values but the characteristics of a device processing this wavelength channel may shift relative to it. A supergrating device may be used to track such deviations and provide feedback to this device, or to a subsequent device attempting to correct the problem.

15

Wavelength drift can be monitored using a 1D supergrating 192 as shown in Figure 6. While light incident at a given input angle on tilted 1D grating 192 will nominally diffract at only a particular output angle, detuning from a central peak-reflectance wavelength will in fact yield a detuning in angle, along with a decrease in diffraction efficiency.

20

This behavior can be used to detect shifts in wavelength, or, assuming the wavelength to be true, shifts in device characteristics which can then be compensated through a variety of mechanisms (e.g. temperature tuning). This may be accomplished by placing photodetectors 193a, 193b symmetrically aligned along the diffraction path of the desired central wavelength; in this configuration, the signal from each will match if local wavelength matches the desired value. (Note that diffraction efficiency will

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normally be intentionally low, so that most power passes through un-deviated.) Deviations in local wavelength are then manifest by a change in the relative values of the photodetectors 193a, 193b, which is monitored by
5 comparator 194. Comparator 194 may determine a difference between the input signals on paths 196, 197, or any suitable sensitivity function may be used, such as a logarithmic subtraction. These deviations can then be corrected for using temperature or any other influencing
10 parameter (not shown).

In alternate embodiments optical BSG 192 characteristics may be programmed and/or tuned through programmable controller 192c and/or tuner 192d, respectively.

Another embodiment of the present invention uses a 2D BSG
15 201 as shown in Figure 7, which may be used to diffract light to the detectors and/or detect drifts in wavelength on several channels simultaneously; or in another embodiment, with a sequence of quasi-1D (i.e. point-source) features 201 etched along a waveguide as shown in
20 Figure 8, which will lead to symmetric diffraction in both lateral directions. A mirror 202 can optionally be etched at one side, for optimal collection of scattered light.

25 Dynamic multi-wavelength equalizer

According to several embodiments of the present invention dynamic equalization of multi-wavelength light may be effected. These embodiments comprise one or more supergratings to attain wavelength-specific optical gain
30 or loss characteristics, and thereby effect equalization.

The dynamic behavior may be attained by utilizing one or more programmable or tunable supergratings.

5 A dynamic multi-wavelength equalizer according to the present invention may be preceded by first routing input wavelengths through a tap-off network monitor that separates channels and monitors their power (see Figures 6 and 7). These signals are sent through processing electronics 194, whose output tunes (or programs) the one
10 or more supergratings of the multi-wavelength equalizer 192B, which equalize the power across channels 191, 191A. Such a configuration may be used as part of a feedback configuration to balance wavelength power.

15 According to some embodiments of the present invention one or more supergratings are used to couple input channels to an output waveguide with lower efficiency for wavelengths whose power must be trimmed. These embodiments may comprise one or more supergrating couplers. Other embodiments of the present invention
20 include using supergrating to impose higher scattering losses for wavelengths whose power must be trimmed.

In alternate embodiments a cascade of BSGs that include "basis functions" can be independently tuned to effect the loss spectrum required for equalization; possible
25 basis functions include step-like spectra that can be shifted relative to one another.

Further alternate embodiments include using a programmable supergrating device whose refractive index features are modified to effect the desired equalization.

30

((

Particular embodiments include: a cascade of co- and counter- directional BSGs (see Figures 2,3,3A, and 4), which successively divide the channels in two sub-bands until individual channels are extracted; and a sequence
5 of tilted single-channel gratings which direct individual channels to their respective output waveguide or detector device (Figure 6, item 193).

Static and Dynamic Add/Drop Filter Embodiment

According to several embodiments of the present invention
10 individual or multiple wavelength channels may be fully or partially spatially separated from an "in" channel and directed to a "drop" channel. Other wavelength channels may be directed from the "in" channel to an "out" channel. Optionally, an "add" channel may be provided,
15 wherein light from the "add" channel may be selectively directed to the "through" channel. Other embodiments may comprise several "drop", "add" or "through" channels. The device functionality in both types of embodiments may be fixed or programmable.

20 Referring to Figure 4A, there is shown a device 4A1 consisting of a set of waveguides 4A3, 4A4 coupled using tunable and/or programmable or fixed counter- and/or co-directional supergrating couplers.

Another embodiment Figure 4B makes use of the Vernier
25 tuning principle, with a design motivated by the principle that the spectral shifts accessible through index tuning are often much less than the total desired tuning range. Multi-channel input enters along one waveguide 4B3, with light coupled to an adjacent
30 waveguide by a multi-peak tunable supergrating 4B2 (with peak spacing generally less than the available tuning

range). A subsequent tunable supergrating 4B6 (generally multi-peak with a different spacing which is also less than the available tuning range) couples a subset of this first set of channels to a third waveguide 4B7. This
5 decimation process can continue as desired, with the supergratings independently tuned relative to one another to drop desired channel(s). The channel selection range can thus greatly exceed the available index-tuned spectral shift.

10 Other embodiments of the present invention include using a two-dimensional or three-dimensional supergrating to direct light into the appropriate channel.

A particular embodiment of the invention can be used to spatially separate all of the wavelength components of an
15 input optical signal.

Lambda Router Embodiment

A Lambda router incorporating features of the present invention is shown in Figure 9. Lambda routers are also known as called wavelength routers, or optical cross-
20 connects (OxCs) - and are devices positioned at network junction points which route wavelength(s) from a specific fiber optic input to another specific fiber optic output. Lambda routers are generally $N \times N$ devices (i.e. with N input fibers I and N output fibers O), with each input
25 fiber typically conveying a single wavelength channel.

Cross/bar operation (i.e. channel light on one waveguide will couple to the other, and vice versa; or will remain on the same waveguide) is achieved by locally tuning and/or programming the supergratings 221A-221F in or out
30 of alignment with the channel wavelength.

Another embodiment of the present invention comprises one or more supergrating couplers to effect the desired routing. Other embodiments comprise one or more add/drop filters.

5

Wavelength Monitor

According to another embodiment of the present invention, a supergrating device may measure the power in one or more optical wavelength channels. Several embodiments of this device comprise one or more supergratings and one or more optical detectors. Alternative embodiments include
10 one or more supergrating couplers or one or more two- or three-dimensional supergratings.

It should be understood that the foregoing description is
15 only illustrative of the invention. Various alternatives and modifications can be devised by those skilled in the art without departing from the invention. Accordingly, the present invention is intended to embrace all such alternatives, modifications and variances that fall
20 within the scope of the appended claims.

CLAIMS

What is claimed is:

1. An optical component comprising at least one optical supergrating, wherein the at least one optical supergrating comprises a quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate optical characteristics in at least one spectral band.

2. An optical coupler comprising:

the optical component as in claim 1, wherein the optical component is adapted to affect at least one chosen optical wavelength;

a first optical waveguide; and

a second optical waveguide, wherein the second optical waveguide is optically coupled to the first optical waveguide via the optical component.

3. A co-directional optical coupler comprising:

the optical coupler as in claim 2, wherein the optical component is adapted to co-directionally couple at least one chosen wavelength.

4. A counter-directional optical coupler comprising:

the optical coupler as in claim 2, wherein the optical component is adapted to counter-directionally couple at least one chosen wavelength.

5. An optical dispersion controller comprising:

a first optical component, wherein the first optical component comprises the optical component as in claim 1, wherein the first optical component is adapted to affect a first chosen wavelength;

a first optical waveguide; and

a second optical waveguide, wherein the second optical waveguide is asymmetric with the first optical waveguide, wherein the first optical waveguide is optically coupled to the second optical waveguide via the first optical component.

6. An optical dispersion controller comprising:

a first optical waveguide;

a second optical waveguide, the second optical waveguide comprising:

an optical component as in claim 1, wherein the optical component is adapted to reflect at least one chosen optical wavelength;

a third optical waveguide; and

an optical circulator, wherein the optical circulator optically couples the first, second, and third optical waveguides.

7. An optical wavelength stability monitor system comprising:

a first optical waveguide comprising:

an optical component as in claim 1, wherein the optical component is adapted to affect at least one chosen optical wavelength;

a plurality of optical detectors, the plurality of optical detectors adapted to receive the affected chosen optical wavelength and generate a plurality of electric signals; and

an electronic processor electrically coupled to the plurality of optical detectors, wherein the electronic processor is adapted to produce an electric signal from the plurality of electric signals.

8. An optical wavelength monitor system as in claim 7 further comprising an optical reflector.

9. A symmetric optical coupler comprising:

the optical component as in claim 1, wherein the optical component is adapted to affect at least one chosen optical wavelength;

a first optical waveguide; and

a second optical waveguide, wherein the second optical waveguide is symmetric with the first optical waveguide, wherein the second optical

waveguide is optically coupled to the first optical waveguide via the optical component.

10. An optical coupler comprising:

a plurality of optical components as in claim 1, wherein the plurality of optical components is adapted to affect at least one chosen optical wavelength;

a first optical waveguide; and

a second optical waveguide, wherein the second optical waveguide is optically coupled to the first optical waveguide via the plurality of optical components, wherein the plurality of optical components are adapted to effect a desired inter-waveguide and intra-waveguide coupling.

11. A method of directing at least one optical signal from a first point to a second point, the method comprising providing an optical component, wherein the optical component comprises at least one optical supergrating, wherein the at least one optical supergrating comprises a quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate optical characteristics in at least one spectral band, and wherein the at least one optical supergrating is adapted to influence the at least one optical signal.

12. A method as in claim 11 further comprising:

providing at least one first optical waveguide;
providing at least one second optical waveguide;
adapting the optical component to affect at least one chosen wavelength; and
optically coupling the at least one chosen wavelength from the at least first optical waveguide to the at least one second optical waveguide via the optical component.

13. A method as in claim 12 wherein providing the at least one first optical waveguide and the at least one second optical waveguides further comprises providing mutually asymmetrical waveguides.

14. A method as in claim 11 further comprising:

providing at least one optical waveguide;
providing at least one second optical waveguide;
adapting the optical component to transmit at least one chosen wavelength; and
optically coupling the at least one chosen wavelength from the at least first optical waveguide to the at least one second optical waveguide via the optical component.

15. A method as in claim 14 wherein providing the at least one first optical waveguide and the at least one second optical waveguides further comprises providing mutually asymmetrical waveguides.

16. A method as in claim 11 further comprising:

providing at least one first optical waveguide
providing at least one second optical waveguide;
providing at least one second optical component,
wherein the at least one second optical component
comprises:

at least one second optical supergrating,
wherein the at least one second optical
supergrating comprises at least one second
quantized refractive index profile, wherein the
at least one second quantized refractive index
profile is adapted to exhibit an at least one
second finite plurality of refractive indexes
adapted to generate an at least one second set
of optical characteristics in at least one
spectral band;

adapting the at least one optical component to
affect at least one chosen wavelength;

adapting the at least one second optical component
to affect the at least one chosen wavelength; and

optically coupling the at least one second optical
waveguide to the at least one first optical
waveguide via the at least one optical component and
the at least one second optical component, wherein
the optical coupling controls intra-waveguide
reflection.

17. A method as in claim 11 further comprising:

providing at least one first optical waveguide;
providing at least one second optical waveguide;

providing at least one third optical waveguide;

providing at least one second optical component,
wherein the at least one second optical component
comprises:

at least one second optical supergrating,
wherein the at least one second optical
supergrating comprises at least one second
quantized refractive index profile, wherein the
at least one second quantized refractive index
profile is adapted to exhibit an at least one
second finite plurality of refractive indexes
adapted to generate an at least one second set
of optical characteristics in at least one
spectral band;

adapting the at least one optical component to
affect at least one chosen wavelength;

adapting the at least one second optical component
to affect the at least one chosen wavelength;

optically coupling the at least one second optical
waveguide to the at least one first optical waveguide via
the at least one optical component; and

optically coupling the at least one third optical
waveguide to the at least one second optical waveguide
via the at least one optical component.

18. A method as in claim 11 further comprising:

providing an optical circulator;

providing at least one first optical waveguide;

providing a second optical waveguide;

providing a third optical waveguide;

adapting the optical component to reflect at least one chosen wavelength; and

arranging the optical circulator to couple the chosen wavelength from the second optical waveguide to the at least one first optical waveguide and from the least one first optical waveguide to the third optical waveguide.

19. A method as in claim 11 further comprising:

providing a plurality of optical detectors for detecting at least one chosen wavelength affected by the optical component, wherein each of the plurality of optical detector outputs an electrical signal corresponding to the chosen wavelength detected by the optical detector; and

coupling each electrical signal to processing electronics.

20. A method of controlling the optical phase characteristics of at least one optical signal, the method comprising:

providing an optical component, wherein the optical component comprises:

at least one optical supergrating, wherein the at least one optical supergrating comprises a quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a

finite plurality of refractive indexes adapted to generate optical characteristics in at least one spectral band; and

adapting the at least one optical component to control the optical phase of the at least one optical signal.

21. A method of processing at least one optical signal comprising:

providing at least one optical component, wherein providing the at least one optical component comprises:

providing at least one optical supergrating, wherein providing the at least one optical supergrating comprises providing a quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate optical characteristics in at least one spectral band; and

adapting the at least one optical component to affect the at least one optical signal.

22. A method as in 21 wherein processing the at least one optical signal further comprises adjusting optical power of at least one wavelength component of the at least one optical signal.

23. A method as in claim 21 wherein processing the at least one optical signal further comprises spatially separating at least one wavelength component.

24. An optical component comprising at least one optical supergrating, wherein the at least one optical supergrating comprises a binary quantized refractive index profile, wherein the binary quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate a reflectance spectrum in at least one spectral band.

25. A method of monitoring the stability of an optical system comprising:

providing at least one optical component,
wherein the at least one optical component
comprises:

at least one optical supergrating, wherein
the at least one optical supergrating
comprises a quantized refractive index
profile, wherein the quantized refractive
index profile is adapted to exhibit a
finite plurality of refractive indexes
adapted to generate optical
characteristics in at least one spectral
band;

providing a plurality of optical detectors;

providing processing electronics; and

adapting the at least one optical component to
affect at least one chosen wavelength component

to interact with the plurality of optical detectors.

26. A programmable optical component comprising at least one optical supergrating, wherein the at least one optical supergrating comprises a quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band.

27. A programmable optical component as in claim 26 further comprising the at least one optical supergrating adapted to change the spectral characteristics in the at least one spectral band.

28. A programmable optical component as in claim 26 further comprising the at least one optical supergrating adapted to change the quantized refractive index profile.

29. A programmable optical component as in claim 26 further comprising at least one thermally responsive optical supergrating adapted to change spectral characteristics in response to thermal energy.

30. A programmable optical component as in claim 26 wherein the optical supergrating is adapted to electro-optic tuning, magneto-optic tuning, electro-strictive tuning, and/or magneto-strictive tuning.

31. A programmable optical component as in claim 26 wherein the optical supergrating is adapted to optical illumination tuning, mechanical straining tuning, and/or current injection tuning.

32. A programmable optical component as in claim 26 wherein the optical supergrating is adapted to electrochromic tuning.

33. A programmable optical component as in claim 26 wherein the optical supergrating is adapted to optical polymer tuning.

34. A programmable optical component as in claim 26 wherein the optical supergrating is adapted to molecular reconfiguration tuning.

35. A programmable optical component as in claim 26 wherein the optical supergrating is adapted to mechanical reconfiguration tuning.

36. An optical component comprising at least one scattering reducing optical supergrating, wherein the at least one scattering reducing optical supergrating comprises:

a quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band; and

at least one grating feature dimension exceeding grating material wavelength $\lambda_{mat} = \lambda_0/n_{eff}$, and a decay constant of the modal tail less than $1/\lambda_{mat}$ in a predetermined region of the at least one scattering reducing optical supergrating.

37. An optical component comprising at least one multi-dimensional optical supergrating, wherein the at least one multi-dimensional optical supergrating comprises a

quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band.

38. A optical component as in claim 37 wherein the at least one multi-dimensional optical supergrating further comprises a two-dimensional distribution of a plurality of optical diffraction pixels.

39. An optical component as in claim 37 wherein the at least one multi-dimensional optical supergrating further comprises a three-dimensional distribution of a plurality of optical diffraction pixels.

40. An optical coupler system for coupling light between waveguides, the optical coupler comprising:

at least one first optical waveguide;

at least one second optical waveguide; and

at least one optical component optically coupling the light from the at least one first optical waveguide to the at least one second optical waveguide, the at least one optical component comprising:

a quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band.

41. An optical coupler system as in claim 40 wherein the at least one first optical waveguide is optically asymmetric with the at least one second optical waveguide.

42. An optical coupler system as in claim 40 wherein the optical coupler system further comprises at least one second optical coupler, wherein the at least one optical coupler and the at least one second optical coupler are adapted to control intra-waveguide reflection.

43. An optical coupler system as in claim 40 wherein the optical coupler system is adapted to couple light counter-directionally to the uncoupled light.

44. An optical coupler system as in claim 40 wherein the optical coupler system is adapted to couple light co-directionally to the uncoupled light.

45. An optical device comprising:

at least one optical waveguide, the at least one optical waveguide comprising:

an optical component for reflecting light within the at least one optical waveguide, the optical component comprising:

a quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band; and

an optical circulator having at least one optical port, wherein the optical circulator is optically coupled to the at least one optical waveguide, wherein the optical circulator is adapted to direct the reflected light to the at least one optical port.

46. An optical dispersion control system comprising:

at least one optical component adapted to generate optical phase characteristics in at least one spectral band, wherein the at least one optical component comprises:

a quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band.

47. An optical dispersion control system comprising:

an optical coupler system for coupling light between waveguides, wherein the optical coupler system is adapted to exhibit wavelength-dependent optical phase characteristics, the optical coupler system comprising:

at least one first optical waveguide;

at least one second optical waveguide; and

at least one optical component optically coupling the light from the at least one first optical waveguide to the at least one second

optical waveguide, the at least one optical component comprising:

a quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band.

48. An optical device for separating wavelength components of an optical signal, the optical device comprising:

at least one optical wavelength separation system, the at least one optical wavelength separation system comprising:

at least one first optical waveguide;

at least one second optical waveguide; and

at least one optical component optically coupling the at least one optical wavelength from the at least one first optical waveguide to the at least one second optical waveguide, the at least one optical component comprising:

a quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band.

49. An optical device as in claim 48 wherein the at least one optical component further comprises a two-dimensional supergrating.

50. An optical device as in claim 48 wherein the at least one optical component further comprises a three-dimensional supergrating.

51. An optical device as in claim 48 further comprising a Vernier separator.

52. A wavelength stability monitor comprising:

 a wavelength monitor comprising:

 at least one optical component comprising:

 a quantized refractive index profile,
 wherein the quantized refractive index
 profile is adapted to exhibit a finite
 plurality of refractive indexes adapted to
 generate spectral characteristics in at
 least one spectral band;

 a plurality of optical detectors coupled to the
 wavelength monitor, wherein the plurality of optical
 detectors are adapted to generate a deviation signal
 when a monitored wavelength deviates; and

 a controller coupled to the plurality of optical
 detectors, wherein the controller is adapted to
 generate an electrical signal corresponding to
 wavelength deviation.

53. A wavelength stability monitor as in claim 52 wherein the at least one optical component comprises a two-dimensional supergrating.

54. A wavelength stability monitor as in claim 52 wherein the at least one optical component comprises a three-dimensional supergrating.

55. A wavelength stability monitor as in claim 52 wherein the at least one optical component comprises an array of point scatters.

56. An optical wavelength equalizer comprising at least one optical component, the at least one optical component comprising a quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band, and wherein the at least one optical component is adapted to adjust wavelength power per wavelength in an optical signal.

57. An optical wavelength equalizer as in claim 56 further comprising an optical coupler system, the optical coupler comprising:

at least one first optical waveguide;

at least one second optical waveguide; and

the at least one optical component optically coupling the adjusted wavelength from the at least one first optical waveguide to the at least one second optical waveguide.

58. An optical wavelength equalizer as in claim 56 wherein the at least one optical component is adapted to diffract chosen wavelengths.

59. An optical wavelength monitor comprising:

at least one optical component, the at least one optical component comprising a quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band, and wherein the at least one optical component is adapted to measure power per wavelength in an optical signal.

60. An optical wavelength monitor as in claim 59 wherein the at least one optical component further comprises a binary supergrating.

61. An optical component comprising at least one programmable optical supergrating.

62. An optical component as in claim 61 wherein the at least one programmable optical supergrating further comprises the at least one optical supergrating adapted to change a quantized refractive index profile.

63. An optical component as in claim 61 wherein the at least one programmable optical supergrating further comprises at least one thermally responsive optical supergrating adapted to change spectral characteristics in response to thermal energy.

64. An optical component as in claim 61 wherein the at least one programmable optical supergrating further comprises the at least one programmable optical supergrating adapted to electro-optic programming, magneto-optic programming, electro-strictive programming, and/or magneto-strictive programming.

65. An optical component as in claim 61 wherein the at least one programmable optical supergrating further comprises the at least one programmable optical supergrating adapted to optical illumination programming, mechanical reconfiguration, mechanical straining programming, and/or current injection programming.

66. An optical component as in claim 61 wherein the at least one programmable optical supergrating further comprises the at least one programmable optical supergrating adapted to electrochromic programming.

67. An optical component as in claim 61 wherein the at least one programmable optical supergrating further comprises the at least one programmable optical supergrating adapted to optical polymer programming.

68. An optical component as in claim 61 wherein the at least one programmable optical supergrating further comprises the at least one programmable optical supergrating adapted to molecular reconfiguration programming.

69. An optical component comprising at least one tuneable optical supergrating, wherein the at least one tuneable optical supergrating comprises a quantized refractive index profile, wherein the quantized refractive index profile is adapted to exhibit a finite plurality of refractive indexes adapted to generate spectral characteristics in at least one spectral band.

70. An optical component as in claim 69 wherein the at least one tuneable optical supergrating is adapted to change a quantized refractive index profile associated with the at least one tuneable optical supergrating.

71. An optical component as in claim 69 wherein the at least one tuneable optical supergrating further comprises at least one thermally responsive optical supergrating adapted to change spectral characteristics in response to thermal energy.

72. An optical component as in claim 69 wherein the at least one tuneable optical supergrating is adapted to electro-optic tuning, magneto-optic tuning, electrostrictive tuning, and/or magneto-strictive tuning.

73. An optical component as in claim 69 wherein the at least one tuneable optical supergrating is adapted to optical illumination tuning, mechanical straining tuning, and/or current injection tuning.

74. An optical component as in claim 69 wherein the at least one tuneable optical supergrating is adapted to electro-chromic tuning.

75. A programmable optical component as in claim 69 further comprising at least one liquid crystal material and/or at least one optical polymer material.

76. An optical component as in claim 69 wherein the at least one tuneable optical supergrating is adapted to mechanical reconfiguration tuning.

77. An optical component comprising at least one optical supergrating, wherein the at least one optical supergrating is adapted to affect optical phase characteristics in at least one spectral band.

78. An optical component as in claim 77 wherein the at least one optical supergrating is adapted to conform to at least one dimension.

79. An optical component as in claim 78 wherein the at least one optical supergrating further comprises an optical supergrating adaptable to programming and/or tuning.

80. An optical coupler comprising:

the optical component as in claim 79, wherein the optical component is adapted to affect at least one chosen optical wavelength;

a first optical waveguide; and

a second optical waveguide, wherein the second optical waveguide is optically coupled to the first optical waveguide via the optical component.

81. An optical dispersion controller comprising:

a first optical component, wherein the first optical component comprises the optical component as in claim 79, wherein the first optical component is adapted to affect a first chosen wavelength;

a first optical waveguide; and

a second optical waveguide, wherein the first optical waveguide is optically coupled to the second optical waveguide via the first optical component.

82. An optical dispersion controller comprising:

a first optical waveguide;

a second optical waveguide, the second optical waveguide comprising:

an optical component as in claim 79, wherein the optical component is adapted to reflect at least one chosen optical wavelength;

a third optical waveguide; and

an optical circulator, wherein the optical circulator optically couples the first, second, and third optical waveguides.

83. An optical wavelength stability monitor system comprising:

a first optical waveguide comprising:

an optical component as in claim 79, wherein the optical component is adapted to affect at least one chosen optical wavelength;

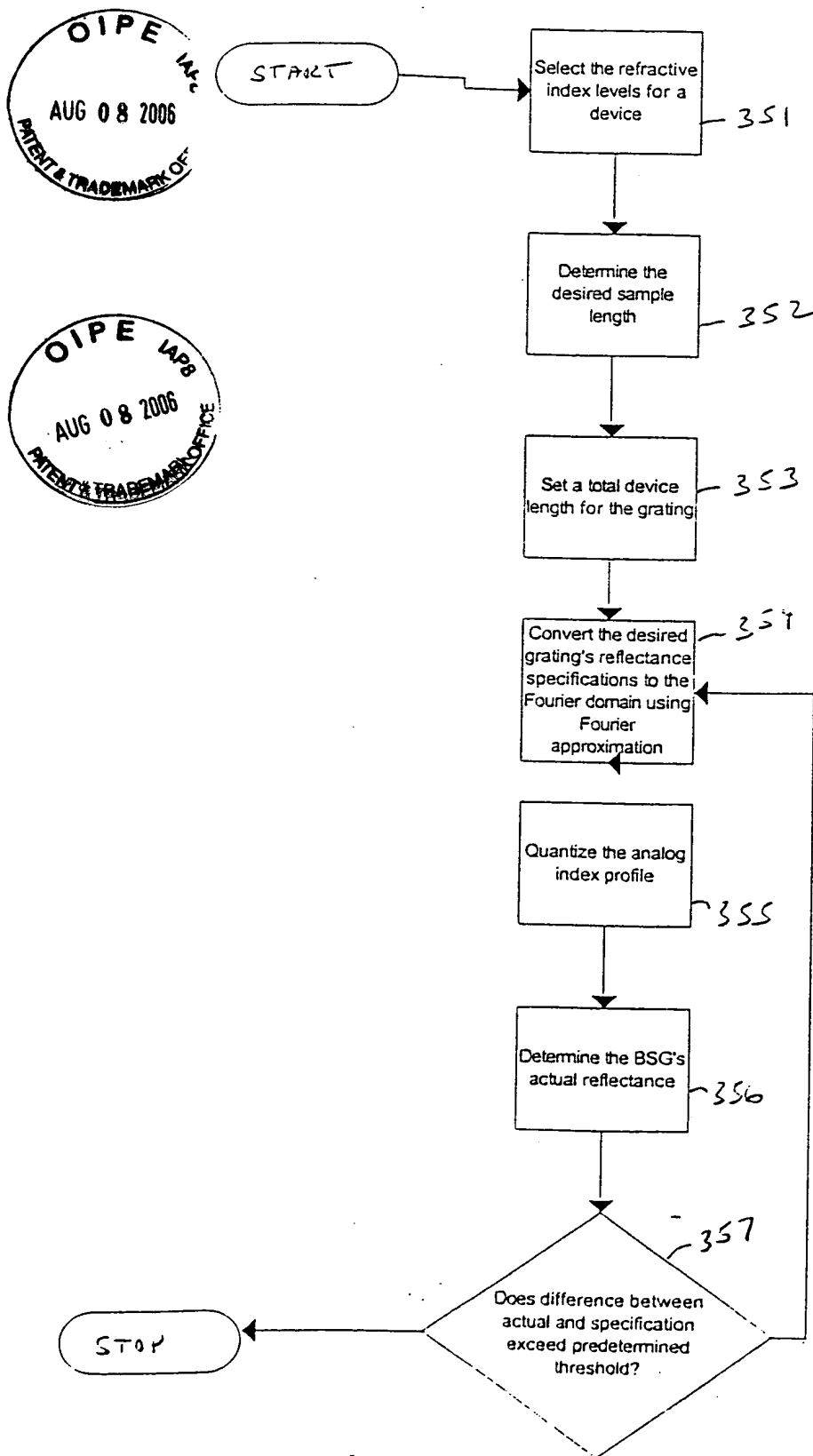
a plurality of optical detectors, the plurality of optical detectors adapted to receive the affected chosen optical wavelength and generate a plurality of electric signals; and

an electronic processor electrically coupled to the plurality of optical detectors, wherein the electronic processor is adapted to produce an electric signal from the plurality of electric signals.

ABSTRACT

An optical component including at least one optical supergrating is provided. The optical supergrating includes a quantized refractive index profile adapted to exhibit a finite plurality of refractive indexes; which in turn are adapted to generate a reflectance spectrum in at least one spectral band corresponding to a Fourier transformed analog refractive index profile.

Figure 1



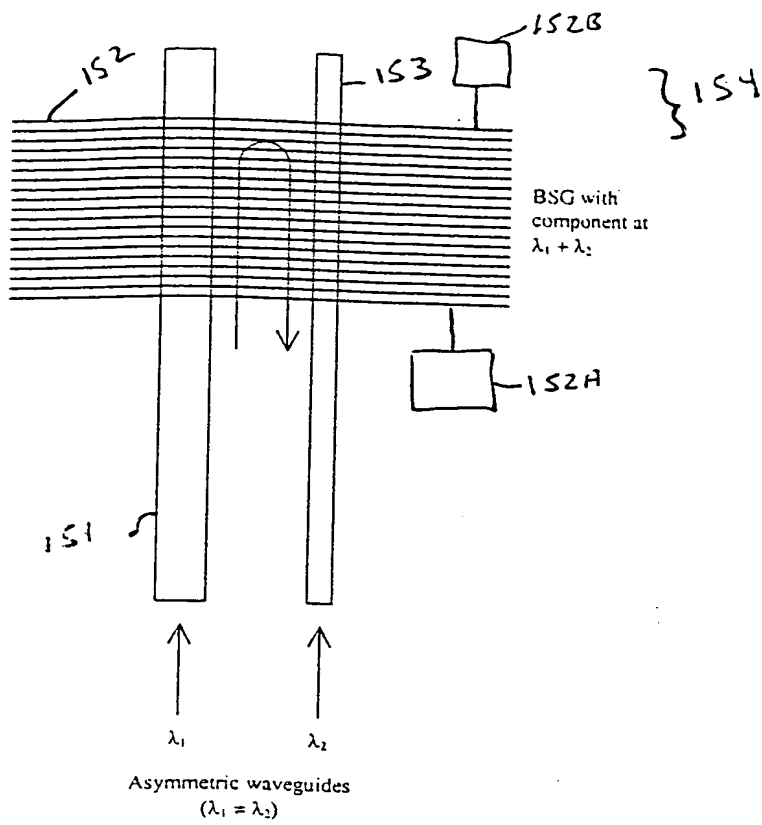


Figure 2

Figure 3

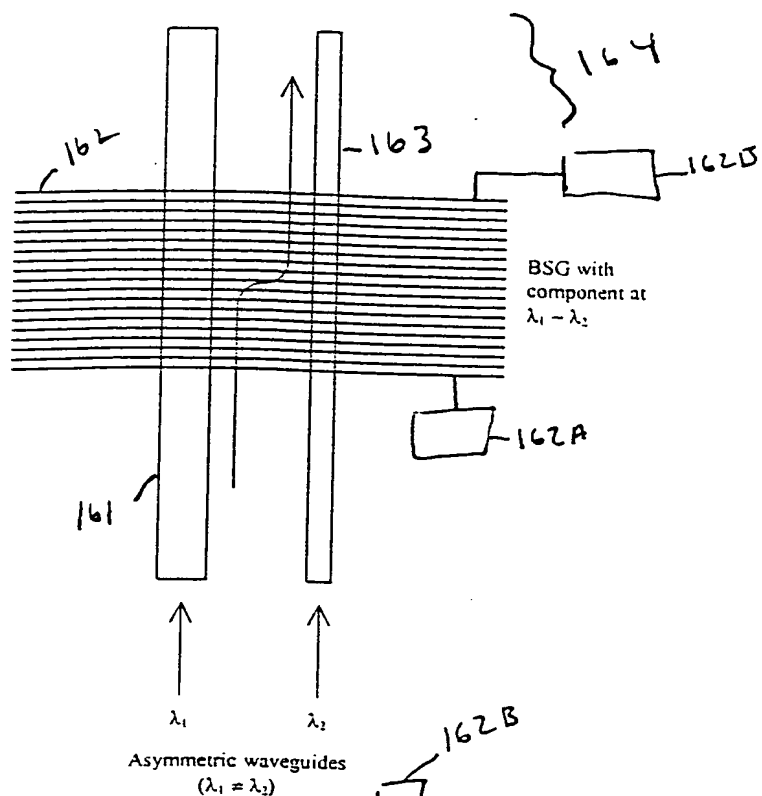


Figure 3A

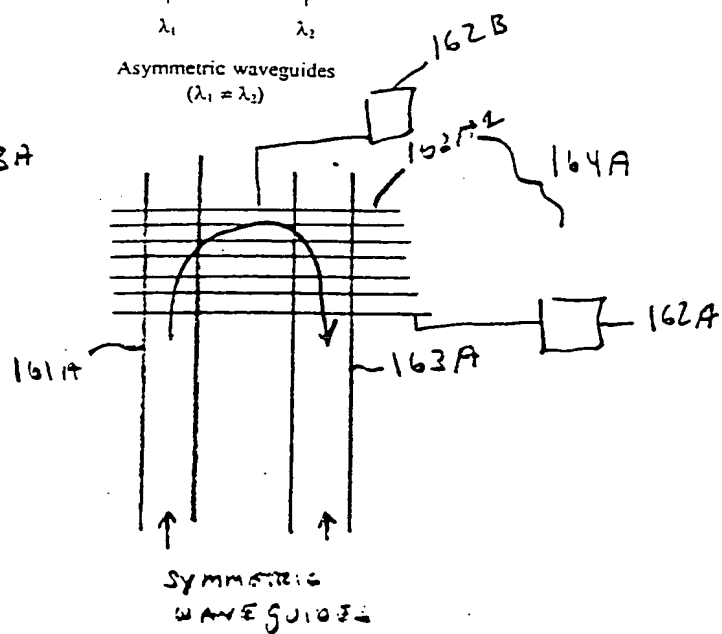


Figure 4

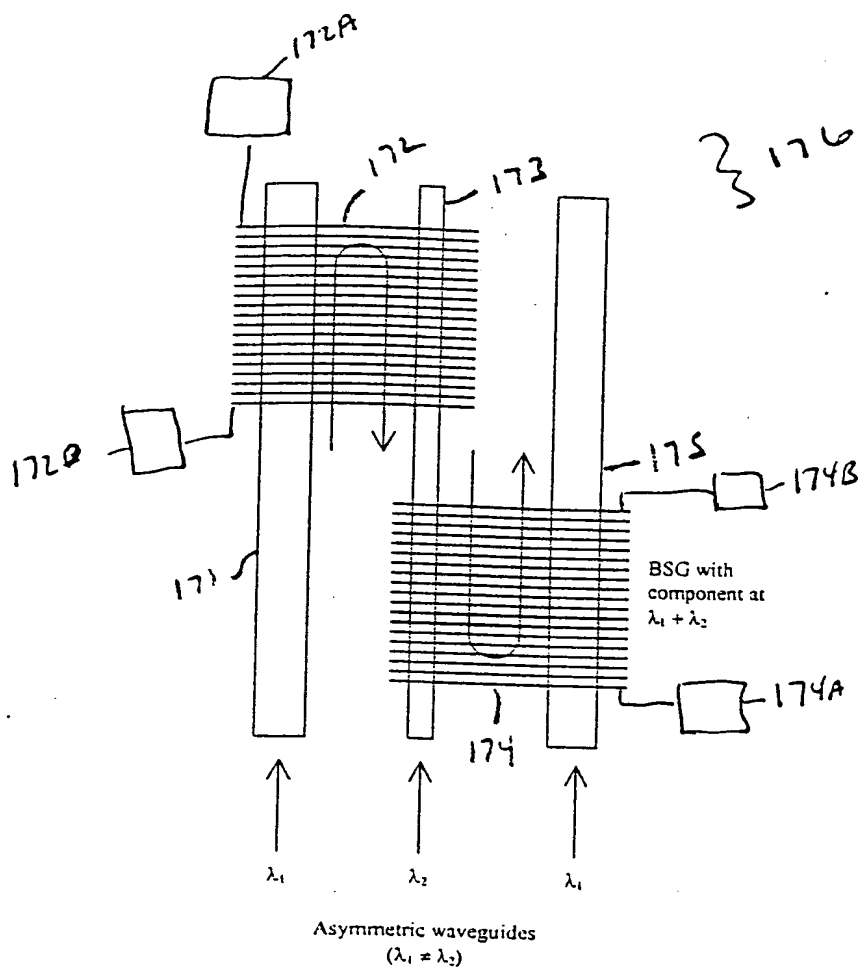


FIGURE 4A

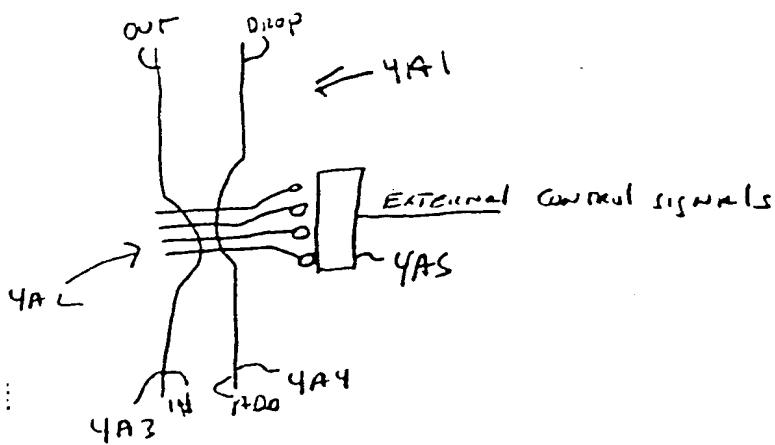
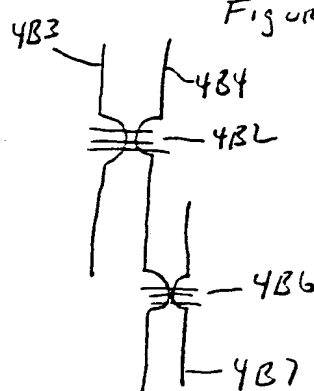


FIGURE 4B



Figure

5

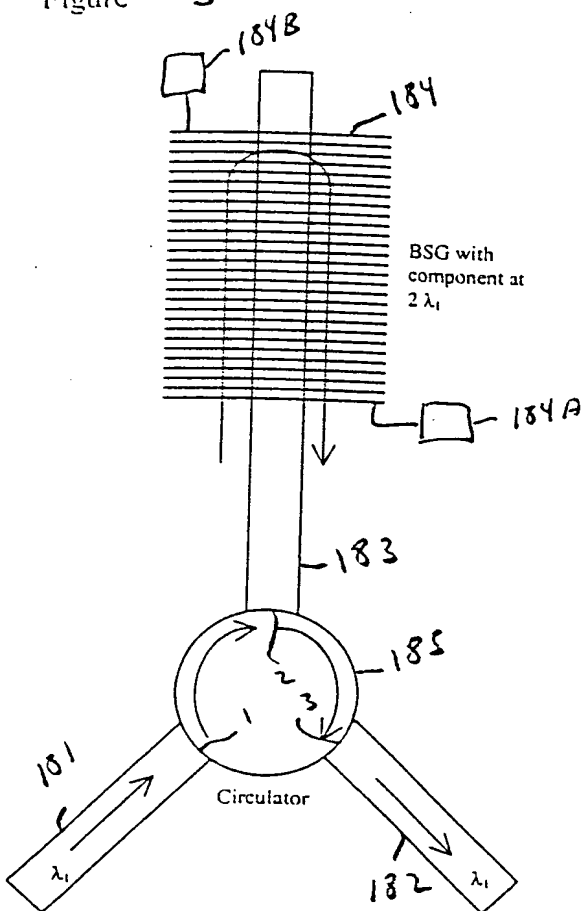


Figure 6

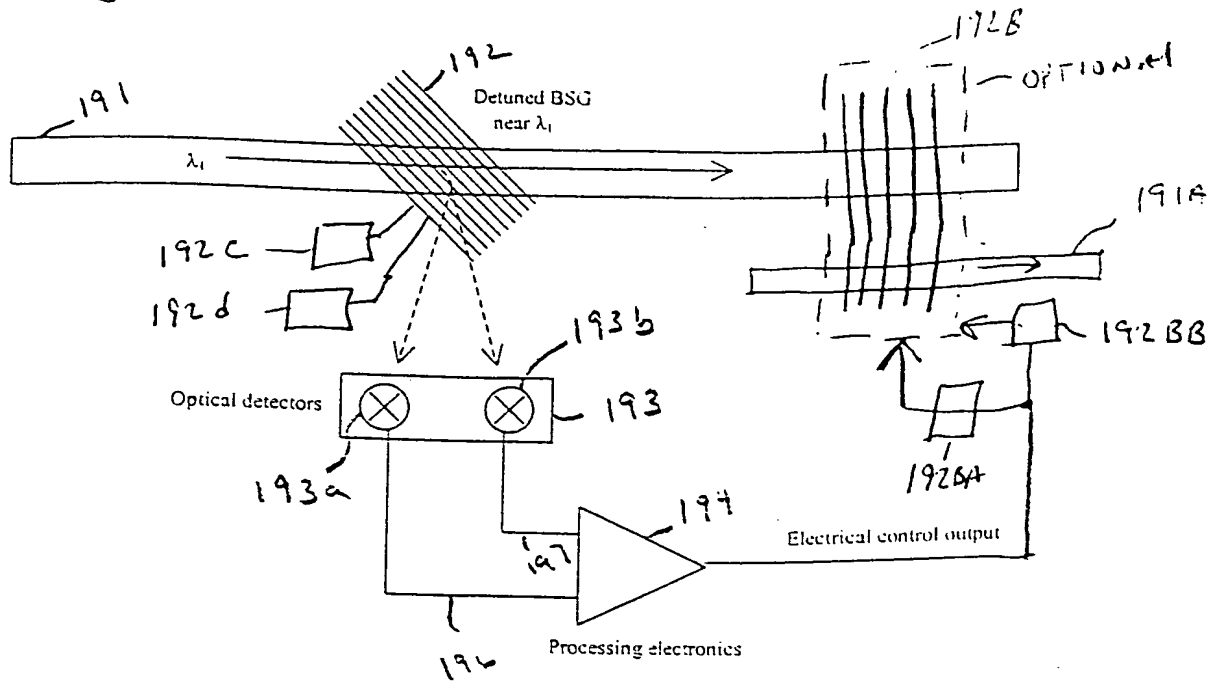


Figure 7

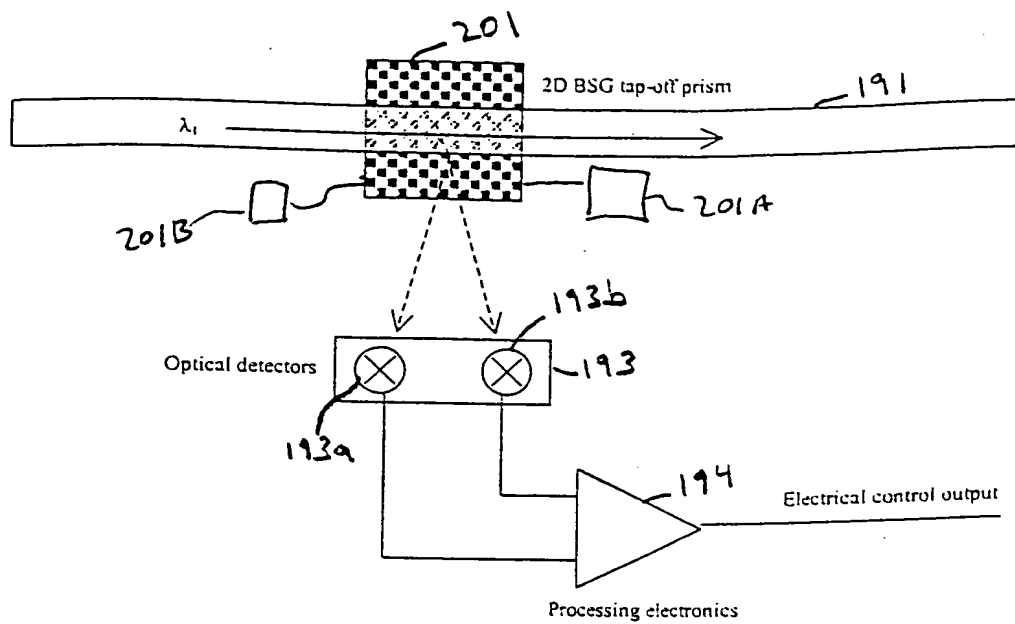


Figure 8

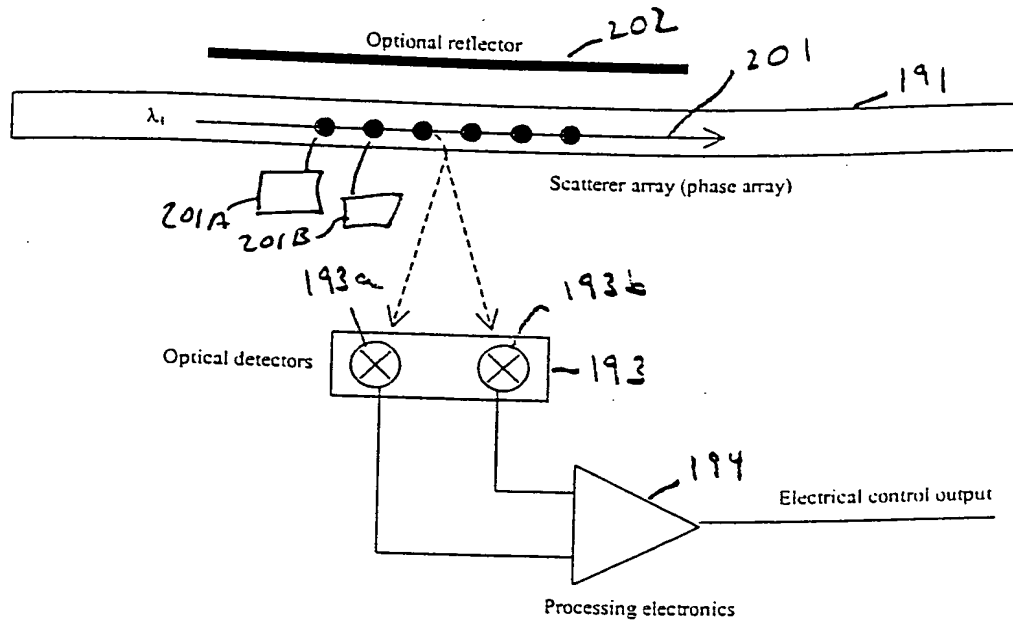
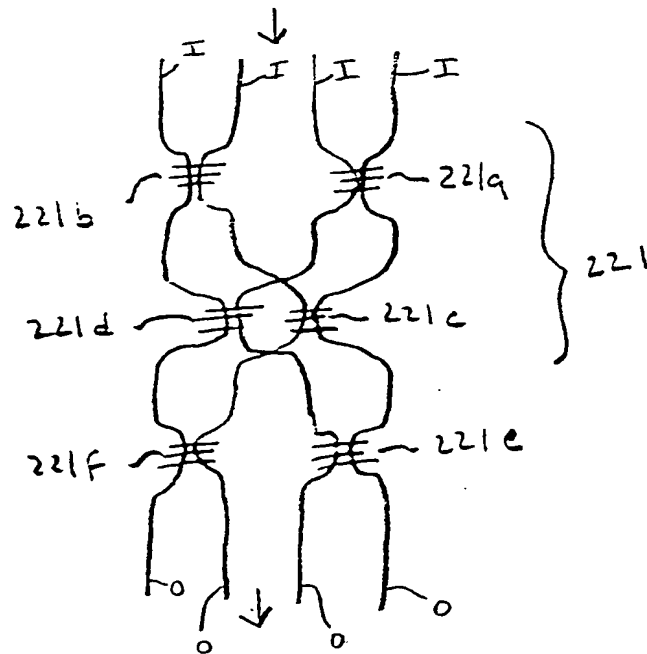


Figure 9



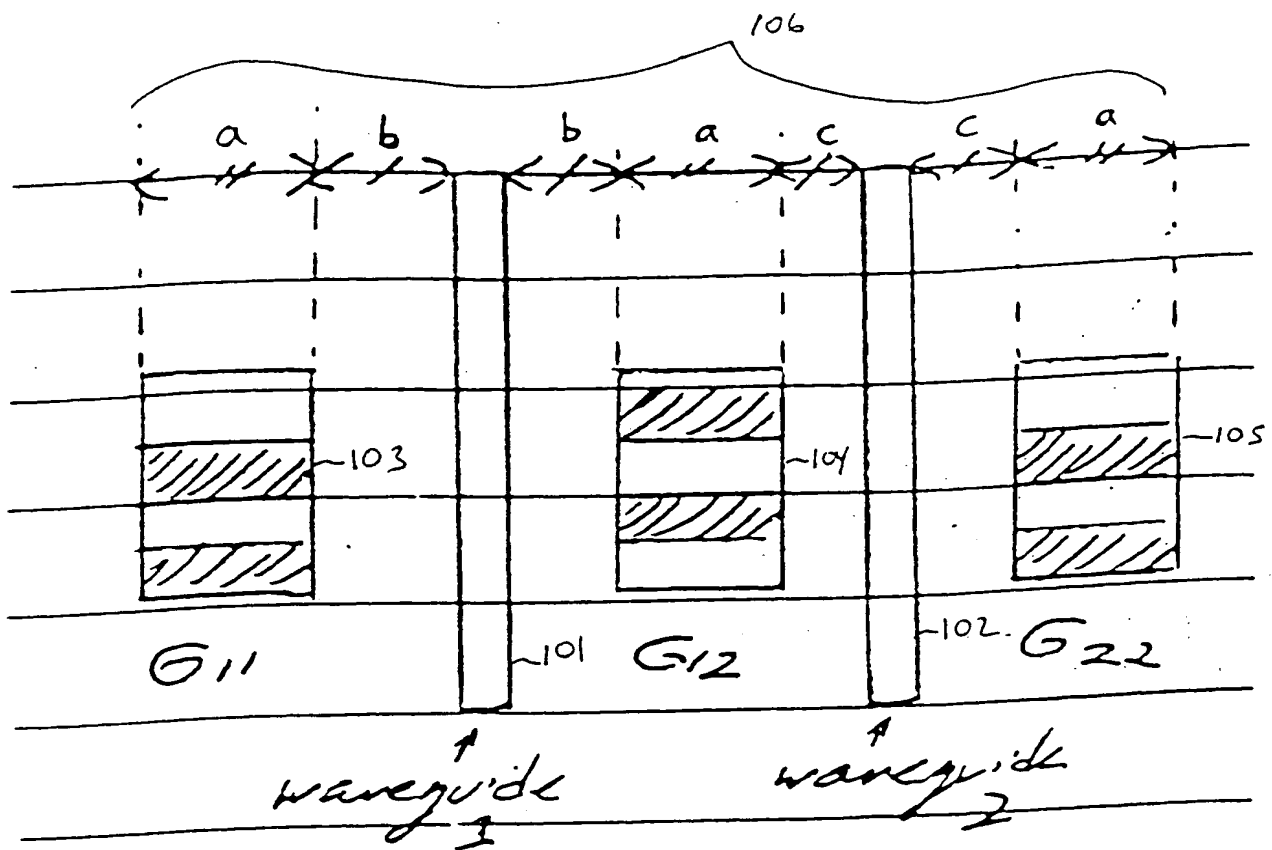


Figure 10